



# Physicochemical and mechanical characterization of Benin's Kenaf fibers and its effect on the building compressed Earth Blocks (CEB) mechanical properties

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## Abstract

The physical, chemical and mineralogical characteristics of Kenaf fibers from the Republic of Benin were studied by using the X-ray diffraction (XRD), infrared spectroscopy (IR), thermal gravimetric analysis coupled with differential scanning calorimetry (TGA/DSC) and chemical analysis using the method of VAN Soest. It emerged from study that the fibers of Kenaf essentially consisted of cellulose (73wt %), hemicelluloses (18 wt%) and lignin (6 wt%). Kenaf fibers of 10, 20 and 30 mm length were used at dose rate of 1.2% weight to reinforce the mechanical and thermal properties of Compressed Earth Blocks (CEB) developed from a clay soil; constituted of kaolinite (33, 46wt%); illite (14.90wt%); microcline (2.11wt%); quartz (48.78wt%) and 0.86wt% of anatase. The incorporation of Kenaf fibers permitted to reduce the distribution of cracks in CEB. Analysis of the mechanical behavior of different formulations soil/fiber in terms of flexural strength and compression demonstrated the beneficial effect of the fibers. The best result of mechanical strength standpoint was obtained with the fibers length of 30 mm. Here we successfully proved that it is possible to improve the mechanical and thermal properties of CEB by using fibers for reinforcement; and the composite can be optimized by altering the fiber content and length.

**Keywords:** Kenaf fibers, Clay soil, Chemical and mineralogical Composition, Mechanical resistance.

## Introduction

Kenaf is an herbaceous plant which annual height is between 1.5 and 3.5 m with a woody base. It belongs to the family of Malvaceae. The diameters of the rods varied from 1 to 2 cm and the leaves, which are of variable sharp, have lengths in the ranging between 100-150 mm. The leaves nearby the stems were strongly lobate (3-7 lobes), whereas the superior nearby stem leaves were slightly lobate. In the Republic of Benin and Burkina Faso, Kenaf leaves are often used to prepare Sauces<sup>1</sup>. White, yellow or purple flowers have diameter varying from 8 to 15 cm. When they are white or yellow, the center is still deeply purple. The fruit is a capsule of 2 cm of diameter containing several seeds. Furthermore, knowing and believing in the high mechanical strength of Kenaf fibers, the latter are often used to produce artisanal bags in West Africa. Benin northern breeders also use Kenaf fibers in the rope in order to attach animals. In Nagoand Yoruba area in the republic of Benin, the earth blocks are traditionally stabilized or reinforced with organic materials available locally such as straws, herbal decoctions and especially cow dung. Many studies have focused on the physical and mechanical characteristics of compressed

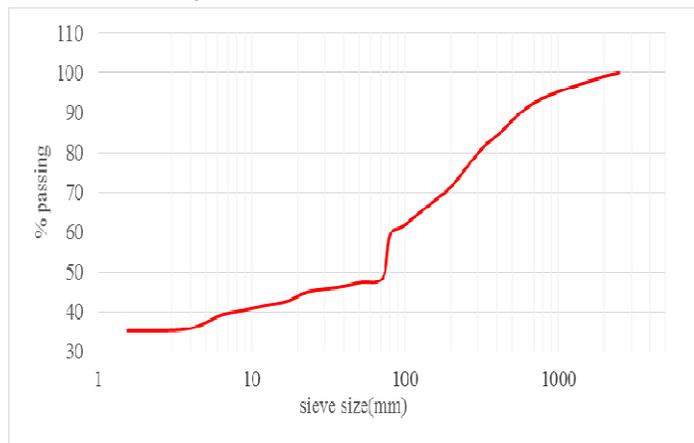
earth blocks stabilized or reinforced with natural fibers<sup>2-11</sup>, but little attention was paid to how the physical and chemical characteristics of fibers incorporated affect physical and mechanical properties of the produced CEB. In addition, the chemical compositions of Kenaf fiber have been in some Asia, South America countries, and Burkina Faso in Africa<sup>11-13</sup>. Despite the fact that their chemical composition is climate, plant species and soil type dependent, any information is available in the literature regarding Benin's Kenaf fibers. Consequently, this work aims at first to study to investigate the properties physical, chemical and mechanical; of Kenaf fibers from the Republic of Benin. Secondly and finally, investigate its impact on the enhancement of the mechanical properties of compressed earth blocks. In short, the main objective of this work is to valorize Kenaf fibers in building earth block fabrication as it is produced and easily available in Benin.

## Materials and methods

**Raw materials:** Kenaf plants were collected from Kandi, a town in northern Benin (West Africa). They were cut at the age of 6 months and retted in rivers and manually defibrated. The

fibers were cut with a massicot to obtain fibers of 10 mm, 20mm or 30 mm length. The soil used were collected from the region of Parakou in northern Benin (between latitudes 9°00' and 10°00' North and longitudes 2°20' and 3°40' East). Figure-1 shows the particle size distribution curve.

**Table-1** presents the geotechnical characteristics of the used land; it was a sandy loam.



**Figure-1:** Grain size distribution of the used soil

**Table-1:** Geotechnical characteristics of the soil sampling area (Parakou town).

| Composition                |                                       |                   |      |
|----------------------------|---------------------------------------|-------------------|------|
| Sand                       |                                       | 61.7 %            |      |
| Limon                      |                                       | 23.5 %            |      |
| Clay (particle size <2 µm) |                                       | 14.8 %            |      |
| Atterberg limits           | Liquid limit LL                       | Norm NF P94-052-1 | 28 % |
|                            | plastic limit PL                      |                   | 14 % |
|                            | plasticity index PI                   |                   | 14 % |
| Other features             | Blue value Norm NF P 94-068           | 1,1               |      |
|                            | Sand equivalent SE Norm NF EN 933-8   | 13                |      |
|                            | Optimum water content Norm NF P94-093 | 12 %              |      |

**Physicochemical, mineralogical and mechanical characterization of fiber:** To assess the mineralogical composition of the fibers, ground fibers (size <80 µm) was used; on which different analysis including X-ray diffraction, thermal gravimetric (TGA) and Fourier transform infrared (FTIR) were performed. Analysis regarding thermal gravimetric was carried out at temperature heating rate of 10°C/min. The diffractometer used was Bruker D 5000 brand apparatus with a graphite rear tube operating with Cu K $\alpha$  radiation. Thermogravimetric curve

up to 1100°C of the fibers was obtained with a SETARAM apparatus at heating rate of 10°C/min. The FTIR analysis was carried out by the mean of Nicolet 510FT-IR spectrometer operating at the wave length of 4000-400 cm<sup>-1</sup>. The fibers for chemical analysis were pulverized in a mortar. The experimental technique used was the Van Soest procedure using four detergents: NDS (Neutral Detergent Soluble) NDF (Neutral Detergent Fiber), ADF (acid detergent fiber) and ADL (Acid Detergent Lignin) to quantify the amount of cellulose, hemicelluloses and lignin<sup>15,16</sup>.

Cellulose is a linear polymer of  $\beta$ - (1-4)-D-glucopyranose, which could be classified into five different types. The first type I is the cellulose with the best physical and mechanical properties (150 GPa Young's modulus). It is a crystalline polysaccharide. The main components of hemicellulose is constituted include saccharides such as xylose, mannose and glucose. It forms a strong block with cellulose fibrils via the multitude of hydrogen bonds. According to Toledo Filho<sup>17</sup>, lignins, as amorphous polymers formed by aromatic units such as guaiacyl, the syringyl and phenylpropane; act as a cementing agent.

The mechanical characterization of Kenaf fibers follows the same methodology as cotton fibers. The fibers are glued on a paper frame of 3.5 cm high and 2 cm wide. The gauge lengths used are 5, 10, 20 and 30 mm. The frame is then placed in the manual clamping jaws of the testing machine (Instron 5566) with a 10 kN cell for monotone uniaxial tensile test. The stress is applied at a constant displacement cross speed (10% l<sub>0</sub> per minute). During the test, the force applied to the sample and the displacement of its point of application (movement of the movable cross member) are recorded.

**Compressed earth blocks (CEB) mechanical characterization:** The flexural and compressive strength were determined accordance to European standard EN 196-1<sup>18</sup>. The measurements were performed on a Zwick mechanical press with a capacity of 50 kN. The 4x4x16cm<sup>3</sup> prism samples were first submitted to a bending test of three points until the rupture in order to assess the flexural stress. The two parts resulting from samples rupture were then recovered and submitted to a single compression test on a plan of 4x4cm<sup>2</sup> area. For Each formulation, we made: three trials of three-point bending tests and six replication of compression test.

**Experimental design:** The compressed earth blocks (CEB) were made using the conventional technic (kneading, compression and release). The dry soil was first coarsely crushed to obtain particles smaller than 5 mm. It is then mixed with sufficient water to achieve the optimum Proctor to obtain maximum compactness after compaction. Kenaf fibers were then added to the mixture. The weight of fiber was fixed at 1.2% of the dry mass of earth. The mixture is then placed in prismatic specimens molds of 4x4x16 cm<sup>3</sup> dimensions. It is then compacted based on the static mode with simple effect by a hydraulic press until a compaction stress of 5 MPa. The test

pieces are demolded after compaction and kept in a conditioned chamber at a temperature of  $20 \pm 1^\circ\text{C}$  and a relative humidity of  $50 \pm 5\%$ . It were then dried until mass stabilization (after 21 days) (Table-2).

## Results and discussion

**Characterization physical chemistry, mineralogy and mechanical of Kenaf fiber compared with flax fibers:** The X-ray diffraction allow to observe the crystal structure of vegetable fibers. The crystalline fraction of vegetable fibers corresponds to one of the polymorphic states of cellulose. Diffractograms of Figure-2 are similar and allow to identify clearly 4 peaks. The peaks at  $15.02$  and  $16.03^\circ$  ( $2\theta$  CuK $\alpha$ ) correspond to the crystallographic planes (110) and (111) of the cellulose I. The main peak at  $22.7^\circ$  corresponds to the plane (002) and finally, the one identified at  $34, 34$  corresponds to the plane (023) or (004). For Kenaf, it is difficult to distinguish the  $15.02$  peak from the one at  $16.03^\circ$ . This reflects a high content of amorphous materials such as lignin, hemicellulose and amorphous cellulose. In contrast, when crystalline cellulose content is high, these two peaks are well separated as observed on flax diffractogram. The crystallinity index of the fibers, corresponds to the ratio of the mass of the crystal phase of cellulose versus the total mass of the sample (cellulose + hemicellulose + pectin + lignin). This crystallinity index was determined for Kenaf and flax fibers based on the method described by Segal *et al.*<sup>19</sup> according to the equation-1 below:

$$I_c = \frac{(I_{002} - I_{AM})}{I_{002}} \quad (1)$$

$I_{002}$  corresponding to the plane (002) of the crystalline phase ( $2\theta = 22.7^\circ$ ) and represents the intensity of both amorphous and crystalline material.  $I_{AM}$  represents the diffraction intensity of the amorphous phase at  $2\theta = 18$  and corresponds only to the intensity of the amorphous portion of the material. In practice,  $I_{AM}$  is the minimum between the diffraction peaks of the planes

{110} and {002} in the crystalline phase. Using the above-mentioned formula, the  $I_c$  values of 49.2 and 77.8 were found respectively for Kenaf and flax crystallinity.

In order to perfect the mineralogical characterization of the CEB and particularly that of amorphous compounds within, milled samples were passed through TGA and FTIR analysis (Figure-3).

During their sintering, the thermal property of the fibers was determined as described by El-Shekeil *et al.*<sup>20</sup> and Morán *et al.*<sup>21</sup>. The profile of samples weight loss as a function of temperature revealed the presence of three characteristic zones:

The first zone (between  $30$  and  $110^\circ\text{C}$ ) marks the elimination of the water initially present in the sample. This fraction is not important because the samples were dried before the test;

The second zone, covering the temperature range from  $210$  to  $400^\circ\text{C}$ , characterized by a significant loss of weight of the samples, corresponds to the active step of fibers pyrolysis. During this stage the main components of fibers (cellulose, hemicellulose and lignin) are degraded. This degradation is characterized by the presence of an exothermic peak around  $335^\circ\text{C}$  at the DSC attributed to the decomposition of the cellulose. This great mass loss indicates that cellulose is an important constituent of fibers. Finally the last area between  $410$  and  $500^\circ\text{C}$  corresponds to the passive step of the pyrolysis of lignin. This area is also marked by the presence of an exothermic peak around  $450^\circ\text{C}$ . The assignment of this peak to the decomposition of lignin is supported the very high thermal resistance of lignin macromolecule. Lignin has great thermal stability due to the possibility of forming hydrogen bonds, which would strengthens the stability of the molecules. Fourier Transform Infrared Spectroscopy is a widely used analytical technique for the identification of chemical bonds characteristics of a given material. The spectra obtained by applying it to Kenaf and flax fibers are shown in Figure-4.

**Table-2:** Experimental design.

| Treatments | Fibers contents | Fibers length [mm] | Mass content of soil water | water content of the mixture | Remark  |
|------------|-----------------|--------------------|----------------------------|------------------------------|---|
| A0         | 0               | -                  | 0%                         | 12 %                         | not bundle reference mixture  |
| A1         | 1.2 %           | 10                 | 0%                         | 11.4%                        |  |
| A2         | 1.2 %           | 20                 | 0%                         | 11.6%                        |   |
| A21        | 1.2 %           | 20                 | 0%                         | 12.5%                        |   |
| A3         | 1.2 %           | 30                 | 0%                         | 11.8%                        |   |

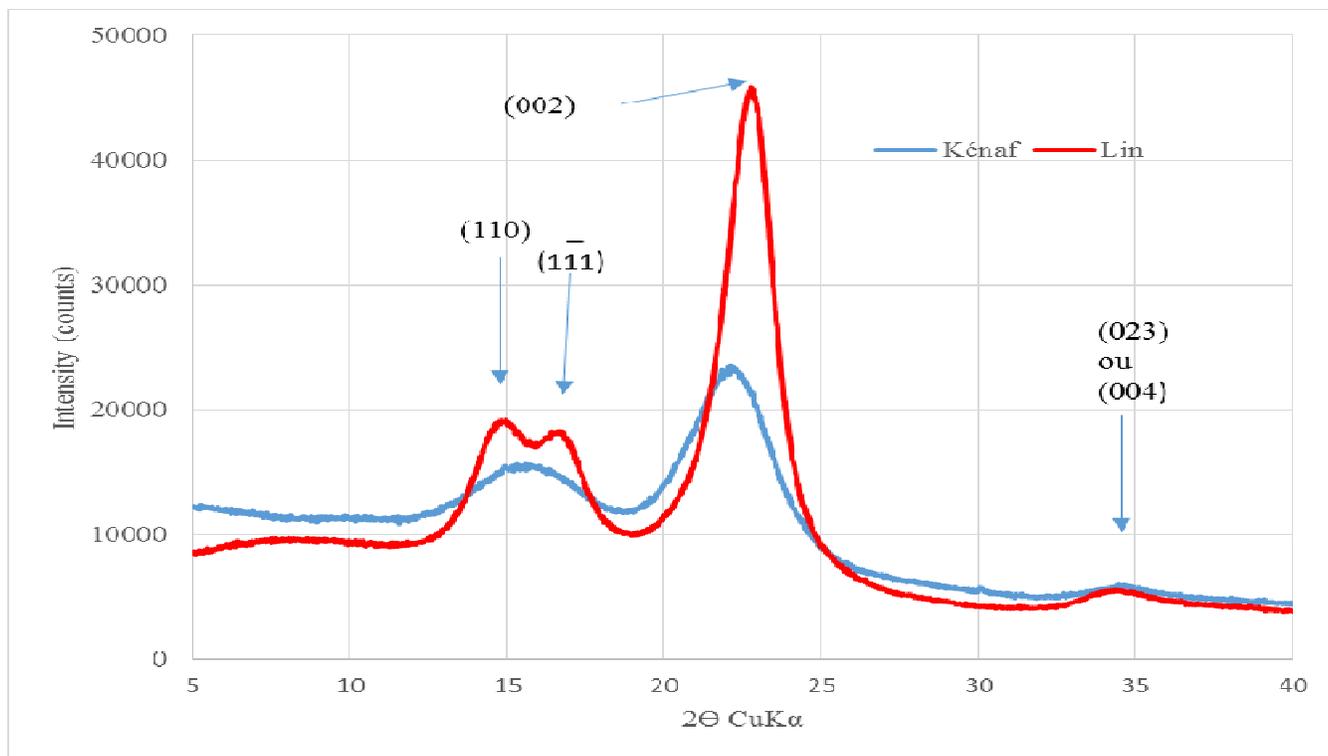


Figure-2: Kenaf fibers diffractogram compared to that of flax.

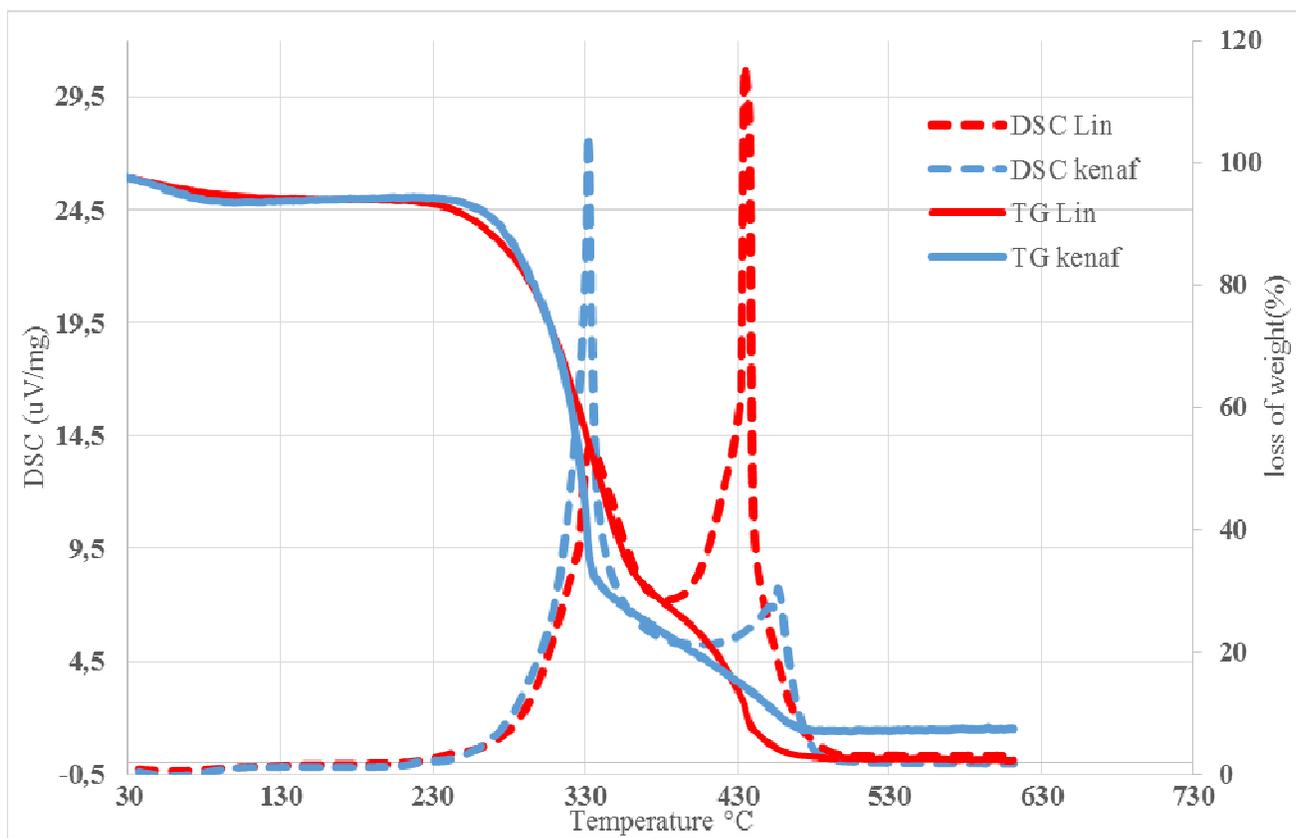
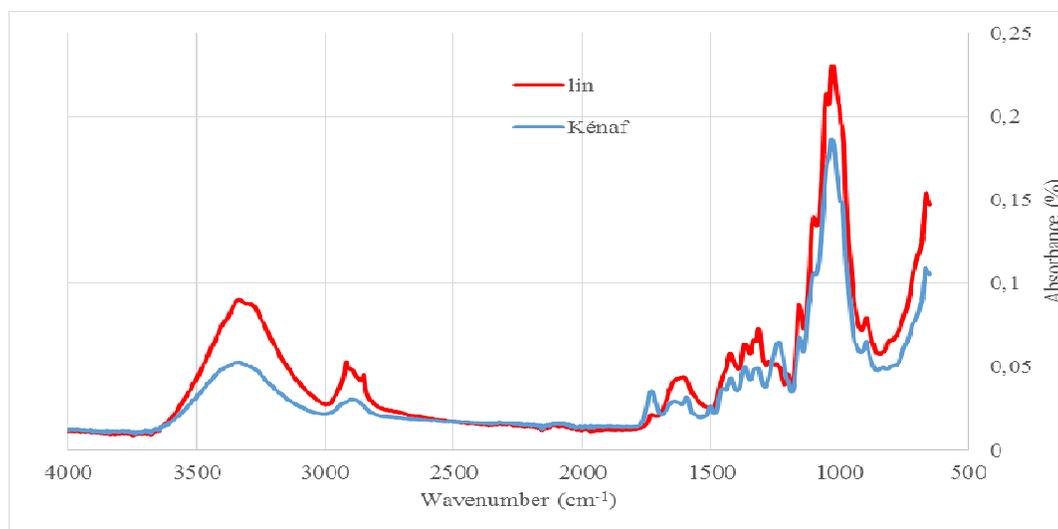


Figure-3: Fiber's TG and DTA curves.



**Figure-4:** Infrared spectrum of Kenaf fibers and flax.

The wide absorption around  $3400\text{ cm}^{-1}$  would correspond to O-H stretching. The same absorption would also characterize absorbed water by the fibers' O-H stretching. The main peaks were identified based on the statement made by Millogo et al.<sup>1</sup>, Ivanova et al.<sup>22</sup>, Morán et al.<sup>21</sup> and Shin et al.<sup>12</sup> as reported in Table-3.

**Table-3:** Main infrared absorption bands Kenaf and flax<sup>1,12,21,22</sup>.

| Wave number $\text{cm}^{-1}$ | Designation  |
|------------------------------|--|
| 3400-3345                    | Characteristic stretching vibrations of O-H bonds of cellulose and hemicellulose                                   |
| 2915                         | Stretching bonds of C-H of cellulose and hemicellulose chains  |
| 2848                         | Stretching of $-\text{CH}_2$ bonds of cellulose and hemicellulose  |
| 1725                         | Stretching of C = O bond of carboxylic acids present in pectins and in acetyl groups present in the hemicelluloses |
| 1625                         | Shear bond vibration-OH characteristic of free water   |
| 1503                         | Cycles aromatiques de la lignine (seulement pour la fibre de Kenaf)  |
| 1420                         | Vibration of the characteristic carbonyl bond pectins  |
| 1360                         | shear vibration of C-H bonds of cellulose and hemicellulose  |
| 1310                         | Stirring of the two H-C bonds of $\text{CH}_2$ -groups of cellulose and hemicellulose                              |
| 1230                         | Characteristic peak of lignin (Kenaf)  |
| 1162                         | Stretching of C-O bonds of acetyl groups (found in hemicellulose or pectins)                                       |
| 1108                         | skew distortion of the group C-O-C   |
| 1032                         | Stretching of the C-O bond   |
| 890                          | characteristic vibration of the $\beta$ binding cellulose  |

Lignin, cellulose and hemicellulose's backbone bands, have been highlighted.

Chemical composition of Kenaf and flax fibers have been compared to other types of fibers (Table-4). It could be seen that the fiber content in hemicelluloses and lignin depends on the origin of the Kenaf material used. Benin's Kenaf fibers cellulose content was in the same order of magnitude as that found in Burkina which was previously studied by Millogo et al<sup>1</sup> (Table-4). This difference between Benin's fibers cellulose contents and others reported in the literature would be explained by the difference in the climate, soil type and plant species. The hemicellulose content was similar to that of Burkina; whereas lignin content is lower than the values available in the literature. The discussion was mainly on cellulose contents, which plays a great role on the mechanical properties of the fibers due to its high tensile strength. The cellulose content of the fibers shown in Table-4 is almost the same for flax, hemp, jute and ramie. Studied Kenaf fibers contained cellulose than that sisal, ramie and jute fibers which emphasized Kenaf high mechanical strength. Figure-5 shows the variation of the average tensile strength of the Kenaf fibers as a function of the gauge length. One can note that the resistance decreases when the gauge length increases. This could be explained by the fact that the rupture occurs by the sudden spread of pre-existing defects and also by the fact that the density and the severity of these defects increase with the tested length. This was in agreement with Mouhoubie<sup>23</sup> and Anthony<sup>24</sup> findings reported on alfa, the diss, and flax fibers, and also synthetic fibers such as glass, carbon<sup>25</sup>. There is also a significant dispersion of the breaking stress. This dispersion may be explained by the fact that the section of those fibers varies along their length. Regardless of the gauge length considered, the average tensile strength of the Kenaf fibers is greater than that of sisal, coconut and palm oil fibers<sup>17-19</sup>. These values are in the same order of magnitude as those obtained by Millogo et al on Kenaf fiber harvested in the Bobo-Dioulasso region (Burkina Faso)<sup>20</sup>.

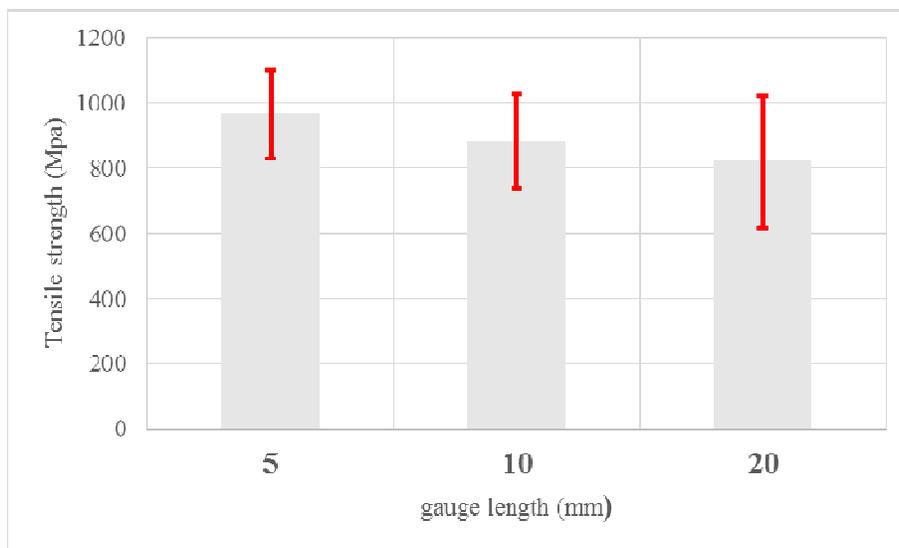


Figure-5: Tensile strength - Influence of the length of the Kenaf fibers.

Table-4: Composition of the fibers and comparison with other types of fibers.

| Fiber                | Cellulose (%) | Hemicellulose (%) | Lignin (%) | Other (compounds water-soluble, waxes, fats, etc) (%) | Reference |
|----------------------|---------------|-------------------|------------|---|-----------|
| <b>Studied Kenaf</b> | <b>73</b>     | <b>18</b>         | <b>6</b>   | <b>1.6</b>  |           |
| Kenaf                | 70            | 19                | 3          | 1.3   | 1         |
|                      | 53±4          | 18±1.4            | 8±1.2      | -   | 30        |
|                      | 45-57         | 21.5              | 8-13       | -   | 14        |
|                      | 58±1          | 22±1              | 17.5±1,3   | 2.4±0.4   | 13        |
|                      | 60.8          | 19.2              | 14.7       | -   | 12        |
|                      | 31-39         | 21.5              | 15-19      | -   | 31        |
| <b>Studied flax</b>  | <b>78.9</b>   | <b>7.3</b>        | <b>4.0</b> | <b>2.6</b>  |           |
| Flax                 | 65-75         | 15                | -          | 2-5   | 32        |
|                      | 71.2          | 18.6              | 2.2        | 6.0   | 33        |
|                      | 67            | 11                | 2          | -   | 33        |
|                      | 80.1          | 14,9              | 3.1        | -   | 34        |
|                      | 82± 3         | 7 ±3              | -          | 5± 2  | 35        |
| Chanvre              | 55            | 16                | 18         | 5   | 36        |
|                      | 74.4          | 17.9              | 3.7        | 0.8   | 37        |
|                      | 56.1          | 10.9              | 6          | 7.9   | 38        |
|                      | 76.12         | 12.28             | 5.65       | 3.29  | 39        |
| Ramie                | 68.6          | 13.1              | -          | -   | 37        |
| Jute                 | 33.4          | 22.7              | 28         | -   | 40        |
|                      | 64.4          | 12                | -          | -   | 37        |
| Sisal                | 70            | 12                | 10         | -   | 41        |
| Coir                 | 33.2          | 31.1              | 20.5       |   | 40        |

**Mechanical properties of compressed earth blocks (CEB):** Figure-6 presents the variation of the flexural strength function of the fiber length. The average values range from 1 to 2 MPa and an important dispersion of the flexural strength values for the treatment A3 it is noticed. This could be explained by the fact that during the preparation of the mixture, the use of low fiber length results in a more homogeneous mixture.

There was also a slight decrease in strength in the treatment A1 compared to A0. This reflects the fact that the fiber length was not sufficient to prevent the propagation of cracks. Furthermore there is a positive effect of the fiber length in treatment A3 showing that  $l = 30$  mm is sufficient to prevent the propagation of cracks. The flexural strength of the reinforced BTC (1.2% Kenaf fiber lengths,  $l = 20$  mm and  $b = 30$  mm), is larger than that of the others values reported in the literature regarding the earth blocks stabilized with fibers<sup>42-44</sup>. This might be due to the

strong tensile stress of Kenaf fibers relative to those used in others studies.

We distinguished three phases in the behavior to flexion of A2 and A3 (Figure-7): Phase I: quasi-linear behavior similar to that of A0, at this stage, efforts are mostly taken up by the matrix as evidenced by the bending energy. There was also a slight increase in the occurrence of the first crack stress compared to A0; Phase II: from  $\sigma^*$ , there was appearance of the first crack of the matrix, followed by the charge resuming by the fibers, which limit the propagation of the crack by a bridging effect; Phase III: beyond  $\sigma_{max}$ , there is a controlled stress reduction unlike A0 which suddenly breaks. This phase is associated with a progressive rupture of fiber/matrix interfaces followed by a loosening of fibers which causes a loss of adhesion between the fibers and the matrix.

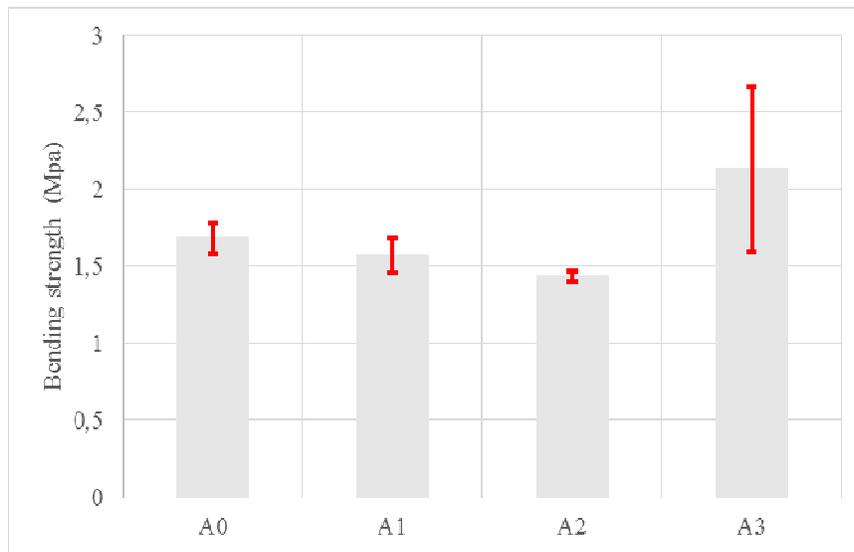


Figure-6: Evolution of the flexural strength in the treatments - Influence of fiber length.

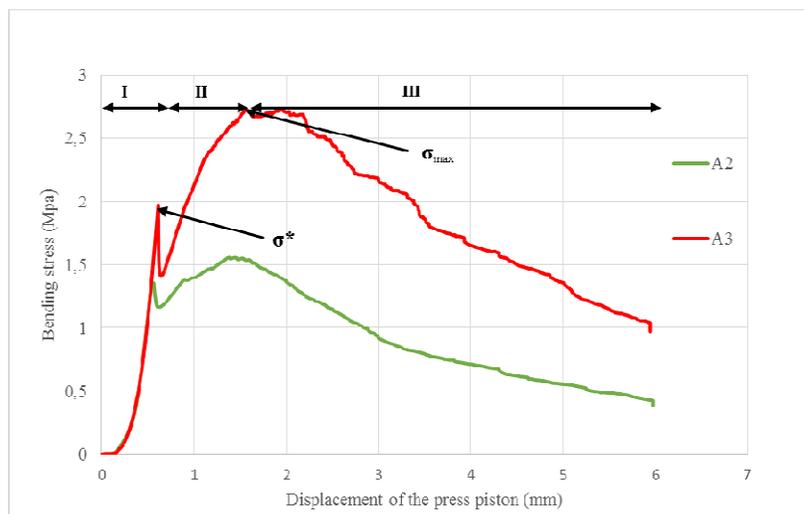


Figure-7: Bending behavior of CEB bundles.

Unreinforced BTC were fragile during bending tests, while those reinforced with fibers have a higher ductility, which is very important for masonry and usually show a brittle behavior. Blocks and mortar higher ductility makes masonry more stable to resist earthquakes and differential settlements, which limits the growth of cracks. In summary, the reinforced BTC ductility's increase erelied on the fibers which hold the cracks after the matrix crack. The resistance strength of the fibers through the cracks is mobilized by their integrated length, where a link is created primarily between cellulose molecules (negatively charged -OH bonds) and, cations such as  $Fe^{3+}$ ,  $Ca^{2+}$

and  $Mg^{2+}$  flocculated within the soil. Figure-8 shows the variation of the compressive strength of BTC for different lengths of fibers. The addition of Kenaf fibers in the ratio of 1.2% dry weight increases the compressive strength of BTC. Furthermore there is an increase of the compressive strength in the treatments A2 compared to A1 and A3. In contract, when considering Figure-9, it appears that, for a deformation of 5%, the strain energy absorbed by the treatment A3 is greater than that absorbed by A1 and A2. This fact led us to conclude that in the mechanical point of view, the formulation A3 is the one having the higher resistance.

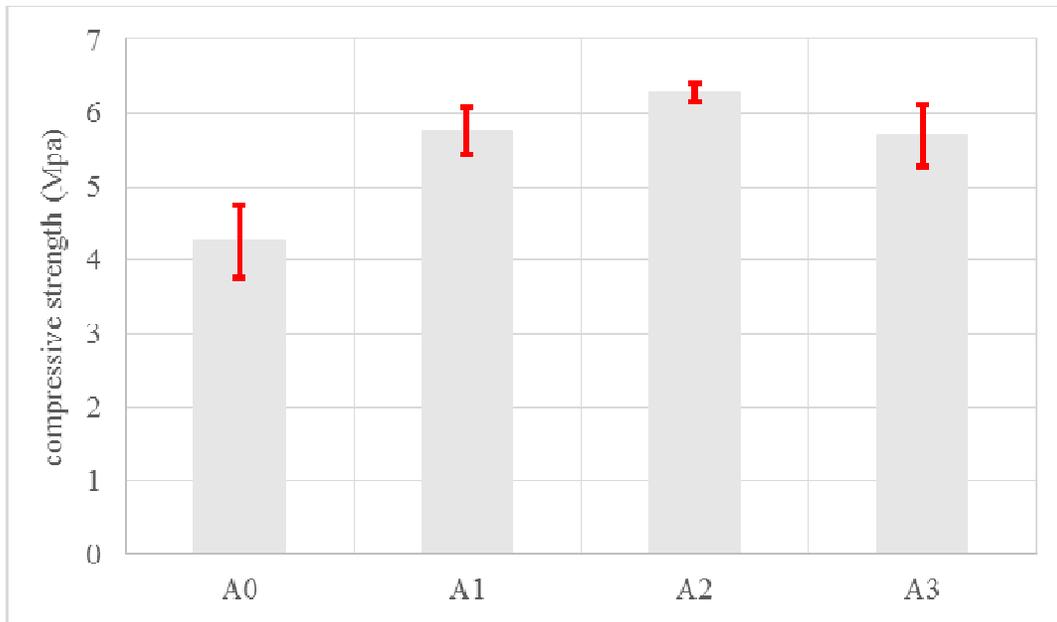


Figure-8: Compressive Strength - Influence of the length of the Kenaf fiber.

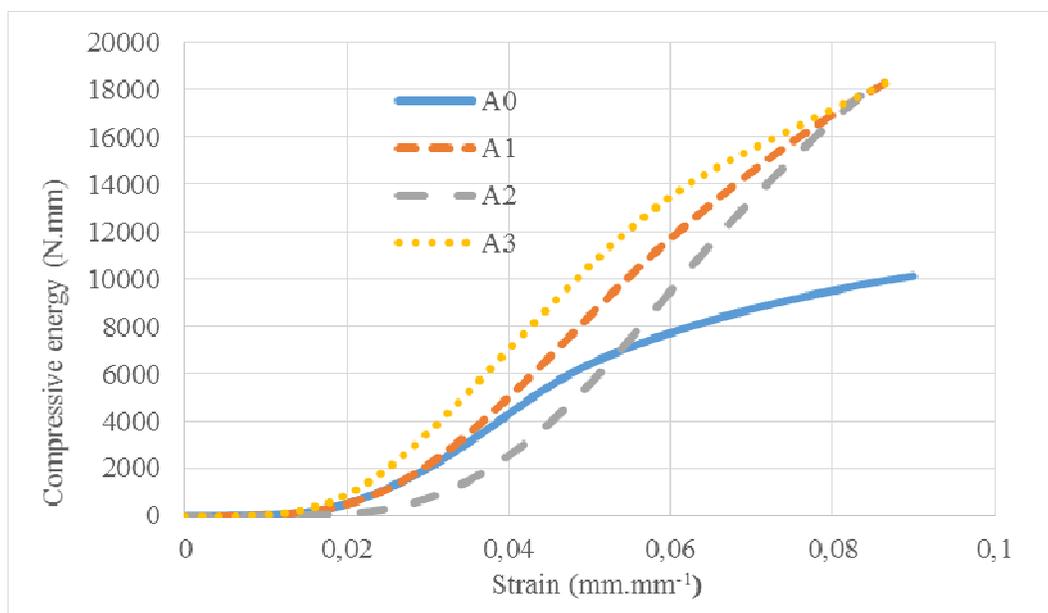


Figure-9: Influence of fiber length on the energy absorbed by the compression CEB.

## Conclusion

Benin's Kenaf fiber physicochemical and mechanical characteristics were determined; and its impact of the mechanical and thermal properties of compressed earth blocks (CEB) were studied. The findings could be summarized as follows: i. The tensile strength of the Kenaf fibers decreases as the gauge length increases and regardless of the gauge length considered the average tensile strength of the Kenaf fibers is greater than the tensile strength of sisal, coconut and oil palm fibers. ii. The studied Kenaf fibers were mainly consisted of cellulose I (73% wt;  $I_c = 49.2$ ), hemicelluloses (18 %wt) and lignin (6%wt). iii. The Addition of Kenaf fibers in earth for compressed earth blocks (CEB) fabrication mainly enhanced the tensile ductility of the blocks; which could be attributed to the high mechanical strength of fibers. iv. The incorporation of Kenaf fibers 30cm is the best treatment as far as mechanical behaviors are concerned.

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